

Generalized solution of a nonlinear optimal control of the heel angle of a rocket

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Abstract: We apply the User's Guide on Dynamics Programming described in [2] to obtain a rigorous and theoretically justified solution of the optimal control problem formulated in [3] as an unsolved problem, and studied in [1] using Pontryagin's Maximum Principle. We use a certain refinement of Cauchy's method of characteristics for stratified Hamilton-Jacobi equations to describe a large set of admissible trajectories and to identify a domain on which the value function exists and is generated by a certain admissible control and, its optimality is justified by the use of one of the well-known verification theorems as an argument for sufficient optimality conditions.

Keywords: Optimal control, differential inclusion, Pontryagin's maximum principle, dynamic programming, Hamiltonian flow.

1 Introduction

The aim of this paper is to apply step by step the dynamic programming theoretical algorithm, described in [2] to obtain a more rigorous and complete theoretically justified solution of the problem formulated as Example 7.3.17 in [3] as an unsolved problem, and studied partially in [1].

2 Position of the problem

The goal of the work [1] is to bring the rocket with a constant mass m to an orbit altitude chosen in advance with a maximum lateral offset. Here, the control represents the heel angle of the rocket. The problem is therefore to determine the optimal trajectory of this rocket. This leads us to solve the optimal control problem of *minimizing* the cost functional:

$$\begin{cases} \min \mathcal{C}(u, T) = -x_1(T), \\ x_1' = v_1, & x_1(0) = 0, \\ x_2' = v_2, & x_2(0) = 0, \\ v_1' = \frac{a}{m} \cos(u(t)), & v_1(0) = 0, \\ v_2' = \frac{a}{m} \sin(u(t)) - g, & v_2(0) = 0, \\ x_2(T) = h, v_1(T) = v_c, v_2(T) = 0, \\ u \in \mathbb{R}, t \in [0, T], T \text{ free}, \end{cases} \quad (1)$$

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such that, $x(t) = (x_1(t), x_2(t))$: the position of the rocket; $v(t) = (v_1(t), v_2(t))$: his speed; $u(t)$: the heel angle of the rocket (which is actually the control function); $a > 0$: is a positive real number representing the Thrust force module; g : the gravitational acceleration.

3 The dynamic programming formulation

problem 1 Given $T, \alpha > 0$, find:

$$\inf_{u(\cdot)} \mathcal{C}(y, u(\cdot)), \forall y \in Y_0 \quad (2)$$

subject to:

$$\begin{aligned} \mathcal{C}(y, u(\cdot)) &= G(x(T)) + \int_0^T f_0(x(t), u(t)) dt, T \text{ free,} \\ x'(t) &= f(x(t), u(t)), u(t) \in U(x(t)) \text{ a.e. } ([0, T]), x(0) = y, \\ x(t) &\in Y_0, \forall t \in [0, T], x(T) \in Y_1, \\ x(\cdot) &= (x_1(\cdot), x_2(\cdot), x_3(\cdot), x_4(\cdot)) = (x_1(\cdot), x_2(\cdot), v_1(\cdot), v_2(\cdot)), \end{aligned} \quad (3)$$

defined by the following data:

$$\begin{aligned} f(x, u) &= (x_3, x_4, \frac{a}{m} \cos u(t), \frac{a}{m} \sin u(t) - g), f_0(x, u) = 0, \\ U(x) &= U = \mathbb{R}, G(\xi) = -\xi_1, \forall \xi = (\xi_1, \xi_2, \xi_3) \in Y_1. \\ Y_0 &= \mathbb{R}_+^4, Y_1 = \mathbb{R}_+^* \times \{(h, v_c, 0)\}. \end{aligned} \quad (4)$$

3.1 Characterization of the Hamiltonian

The first step of the Dynamic Programming Approach consists in characterization of the true Hamiltonian of the problem. The pseudo-Hamiltonian $\mathcal{H}(x, p, u) = \langle p, f(x, u) \rangle + f_0(x, u)$ is given in our case by:

$$\begin{aligned} \mathcal{H}(x, p, u) &= p_1 x_3 + p_2 x_4 - g p_4 + \frac{a}{m} \phi(u), \\ \phi(u) &= p_3 \cos u + p_4 \sin u. \end{aligned} \quad (5)$$

The Hamiltonian and the corresponding multifunction of minimum points are given by the formulas:

$$\begin{aligned} H(x, p) &= \min_{u \in U} \mathcal{H}(x, p, u) = p_1 x_3 + p_2 x_4 - g p_4 + \frac{a}{m} \min_{u \in U} \phi(u), \\ \widehat{U}(x, p) &= \{u \in U; \mathcal{H}(x, p, u) = H(x, p)\}, \end{aligned} \quad (6)$$

Therefore, the Hamiltonian function as well as the corresponding multifunction of minimum points turn out to be defined on Z by:

$$\begin{aligned} H(x, p) &= p_1 x_3 + p_2 x_4 - g p_4 + \frac{a}{m} \phi(\widehat{u}(p)), (x, p) \in Z \\ \widehat{u}(p) &= \begin{cases} \arctan \frac{p_4}{p_3}, & \text{if } \begin{cases} p_3 < 0, p_4 < 0 \\ p_3 + p_4 < 0, p_3 > 0 \\ p_3 + p_4 < 0, p_4 > 0 \end{cases} \\ \frac{\pi}{2}, & \text{if } p_3 = 0, p_4 < 0 \\ \frac{3\pi}{2}, & \text{if } p_3 = 0, p_4 > 0 \end{cases} \end{aligned} \quad (7)$$

First, we remark that the Hamiltonian $H(\cdot, \cdot)$ as well as its domain Z are \mathcal{C}^1 -stratified by the stratification $S_H = \{Z_{-, -}, Z_{+, -}, Z_{-, +}, Z_{0, \pm}\}$ defined by:

$$\begin{aligned} Z_{-, -} &= \{(x, p) \in Z; p_3 < 0, p_4 < 0\} \\ Z_{+, -} &= \{(x, p) \in Z; p_3 + p_4 < 0, p_3 > 0\} \\ Z_{-, +} &= \{(x, p) \in Z; p_3 + p_4 < 0, p_4 > 0\} \\ Z_{0, \pm} &= \{(x, p) \in Z; p_3 = 0, p_4 \in \mathbb{R}^{\pm}\}. \end{aligned} \quad (8)$$

Set of terminal transversality points

Next, we need to compute the set of terminal transversality values defined in the general case by:

$$Z^* = \{(\xi, q) \in Y_1 \times \mathbb{R}^4, H(\xi, q) = 0, \langle q, \bar{\xi} \rangle = DG(\xi)\bar{\xi} \forall \bar{\xi} \in T_{\xi}Y_1\}.$$

Lemma 1. *The set of terminal transversality values Z^* in our case is given by the formulas:*

$$\begin{aligned} Z^* &= Z_{-,-}^* \cup Z_{+,-}^* \cup Z_{0,-}^* \\ Z_{-,-}^* &= \left\{ \left(\left(\xi_1, h, -\frac{a}{m} \sqrt{q_3^2 + q_4^2} - gq_4, 0 \right), (-1, q_2, q_3, q_4) \right); \right. \\ &\quad \left. \xi_1 > 0, q_2 \in \mathbb{R}, q_3 < 0, q_4 < \frac{a}{\sqrt{m^2 g^2 - a^2}} q_3 \right\} \\ Z_{+,-}^* &= \left\{ \left(\left(\xi_1, h, \frac{a}{m} \frac{q_3^2 - q_4^2}{\sqrt{q_3^2 + q_4^2}} - gq_4, 0 \right), (-1, q_2, q_3, q_4) \right); \right. \\ &\quad \left. \xi_1 > 0, q_2 \in \mathbb{R}, q_3 + q_4 < 0, q_3 > 0 \right\} \\ Z_{0,-}^* &= \left\{ \left(\xi_1, h, \left(\frac{a}{m} - g \right) q_4, 0 \right), (-1, q_2, 0, q_4); \xi_1 > 0, q_2 \in \mathbb{R}, q_4 < 0 \right\} \end{aligned} \tag{9}$$

4 Generalized Hamiltonian and characteristic flow

The first main computational operation consists in the backward integration (for $t \leq 0$), of the Hamiltonian inclusion:

$$(x', p') \in d_S^{\#}H(x, p), (x(0), p(0)) = z = (\xi, q) \in Z^*, \tag{10}$$

defined by the generalized Hamiltonian field $d_S^{\#}H(., .)$:

$$\begin{aligned} d_S^{\#}H(x, p) &= \{ (x', p') \in T_{(x,p)}Z; x' \in f(x, \widehat{U}(x, p)), \\ &\quad \langle x', \bar{p} \rangle - \langle p', \bar{x} \rangle = DH(x, p)(\bar{x}, \bar{p}), \forall (\bar{x}, \bar{p}) \in T_{(x,p)}Z \}. \end{aligned} \tag{11}$$

As it is specified in the algorithm given in [2], for each terminal point $z = (\xi, q) \in Z_1^*$ one should identify the maximal solutions: $X^*(.) = (X(.), P(.)) : I(z) = (t^-(z), 0] \rightarrow Z$, of the Hamiltonian inclusion satisfy the following conditions:

$$\begin{aligned} X(t) &\in Y_0, \forall t \in I_0(z) = (t^-(z), 0) \\ H(X(t), P(t)) &= 0, \forall t \in I(z) \\ X'(t) &= f(X(t), u(t)), u(t) \in \widehat{U}(X^*(t)) \text{ a.e. } I_0(z). \end{aligned} \tag{12}$$

Since the manifolds $Z_{-,-}, Z_{+,-} \subset Z$, are open subsets, one has:

$$\begin{aligned} d_S^{\#}H_{-,-}(x, p) &= \left\{ \left(\frac{\partial H_{-,-}}{\partial p}(x, p), -\frac{\partial H_{-,-}}{\partial x}(x, p) \right) \right\}, (x, p) \in Z_{-,-} \\ d_S^{\#}H_{+,-}(x, p) &= \left\{ \left(\frac{\partial H_{+,-}}{\partial p}(x, p), -\frac{\partial H_{+,-}}{\partial x}(x, p) \right) \right\}, (x, p) \in Z_{+,-}. \end{aligned} \tag{13}$$

The Hamiltonian system on the stratum $Z_{-,-}$

On the open stratum $Z_{-,-}$ for which $p_3 < 0, p_4 < 0$, the differential inclusion coincides with the nonlinear Hamiltonian system:

$$\begin{cases} (x'_1, x'_2, x'_3, x'_4) = \left(x_3, x_4, -\frac{a}{m} \frac{p_3}{\sqrt{p_3^2 + p_4^2}}, -\frac{a}{m} \frac{p_4}{\sqrt{p_3^2 + p_4^2}} - g \right) \\ (p'_1, p'_2, p'_3, p'_4) = (0, 0, -p_1, -p_2). \end{cases} \tag{14}$$

The Hamiltonian system on the stratum $Z_{+,-}$

On the open stratum $Z_{+,-}$ for which $p_3 + p_4 < 0$, $p_3 > 0$, the differential inclusion coincides with the nonlinear Hamiltonian system:

$$\begin{cases} (x'_1, x'_2, x'_3, x'_4) = \left(x_3, x_4, \frac{a}{m} \frac{p_3[p_3^2 + 3p_4^2]}{(p_3^2 + p_4^2)^{\frac{3}{2}}}, -\frac{a}{m} \frac{p_4[p_4^2 + 3p_3^2]}{(p_3^2 + p_4^2)^{\frac{3}{2}}} - g \right) \\ (p'_1, p'_2, p'_3, p'_4) = (0, 0, -p_1, -p_2). \end{cases} \quad (15)$$

The Hamiltonian flow ending on the stratum $Z_{-,-}$

From the dynamic programming algorithm in [2], it follows that, we must retain only the trajectories $X_{-,-}^*(\cdot, z)$, $z = (\xi, q) \in Z_{-,-}^*$, that satisfy the conditions:

$$\begin{aligned} X_{-,-}^*(t, z) &= (X^{-,-}(t, z), P^{-,-}(t, z)) \in Z_{-,-}, \forall t \in (\tau^{-,-}(z), 0) \\ H_{-,-}(X_{-,-}^*(t, z)) &= 0, X^{-,-}(t, z) \in Y_0, \end{aligned} \quad (16)$$

on the maximal intervals $I^{-,-}(z) = (\tau^{-,-}(z), 0)$, hence the extremity $\tau^{-,-}(\cdot)$ is defined by:

$$\begin{aligned} \tau^{-,-}(z) &= \max \left\{ \tau_1^{-,-}(z), \tau_2^{-,-}(z) \right\}, \\ \tau_1^{-,-}(z) &= \inf \left\{ \tau < 0; P_3^{-,-}(t, z) < 0, P_4^{-,-}(t, z) < 0, \forall t \in (\tau, 0) \right\} \\ \tau_2^{-,-}(z) &= \inf \left\{ \tau < 0; X^{-,-}(t, z) \in Y_0, \forall t \in (\tau, 0) \right\}. \end{aligned} \quad (17)$$

Further, the second component of the hamiltonian flow $X_{-,-}^*(\cdot, \cdot)$ is given by the formulas:

$$\begin{aligned} P^{-,-}(t, q_2, q_3, q_4) &= (-1, q_2, -t + q_3, -q_2t + q_4), \quad q_2 \in \mathbb{R}, \quad q_3 < 0, \\ q_4 &< \frac{a}{\sqrt{m^2g^2 - a^2}} q_3, \end{aligned} \quad (18)$$

Also, the extremity $\tau_1^{-,-}(\cdot)$ is given by the formulas:

$$\tau_1^{-,-}(q_2, q_3, q_4) = \begin{cases} \max \left\{ q_3, \frac{q_4}{q_2} \right\}, & \text{if } q_2 > 0, \quad q_3 < 0 \\ q_3, & \text{if } q_2 \leq 0, \quad q_4 < \frac{a}{\sqrt{m^2g^2 - a^2}} q_3. \end{cases} \quad (19)$$

The Hamiltonian flow ending on the stratum $Z_{+,-}$

On the stratum $Z_{+,-}$ the maximal interval $I^{+,-}(\cdot)$ is of the same form as in above, where the extremity $\tau_1^{+,-}(\cdot)$ is defined in this case as:

$$\tau_1^{+,-}(z) = \inf \left\{ \tau < 0; P_3^{+,-}(t, z) + P_4^{+,-}(t, z) < 0, P_3^{+,-}(t, z) > 0, \forall t \in (\tau, 0) \right\}. \quad (20)$$

The extremity $\tau_1^{+,-}(\cdot)$ is given by the formulas:

$$\tau_1^{+,-}(q_2, q_3, q_4) = \begin{cases} \frac{q_3 + q_4}{q_2 + 1}, & \text{if } q_2 > -1, \quad q_3 + q_4 < 0, \quad q_3 > 0 \\ -\infty & \text{if } q_2 \leq -1, \end{cases} \quad (21)$$

4.1 Value function and optimal trajectories

The natural candidate for value functions and optimal controls in *Problem 1* are the extreme ones, defined by the next maximization process:

$$\begin{aligned}
 W(x) &= \begin{cases} g(x) = -x_1, & \text{if } x \in Y_1 \\ W_0(x) = \inf_{X(t,b)=x} V(t,b), & \text{if } x \in X(B_0) \subset Y_0 \end{cases} \\
 \widehat{B}(x) &= \{(t,b) \in B; X(t,b) = x, V(t,b) = W_0(x)\}
 \end{aligned} \tag{22}$$

Lemma 2. (1) *The mapping $X^{-, -}(\cdot, \cdot, \cdot, \cdot, \cdot) : B^{-, -} \rightarrow Y_0^{-, -}$ is a diffeomorphism whose inverse $\widehat{B}^{-, -}(\cdot)$ is described by:*

$$\widehat{B}^{-, -}(x) = (\widehat{t}^{-, -}(x), \widehat{\xi}_1^{-, -}(x), \widehat{q}_2^{-, -}(x), \widehat{q}_3^{-, -}(x), \widehat{q}_4^{-, -}(x)), x \in Y_0^{-, -}. \tag{23}$$

(2) *The mapping $X^{+, -}(\cdot, \cdot, \cdot, \cdot, \cdot) : B^{+, -} \rightarrow Y_0^{+, -}$ is a diffeomorphism whose inverse $\widehat{B}^{+, -}(\cdot)$ is described by:*

$$\widehat{B}^{+, -}(x) = (\widehat{t}^{+, -}(x), \widehat{\xi}_1^{+, -}(x), \widehat{q}_2^{+, -}(x), \widehat{q}_3^{+, -}(x), \widehat{q}_4^{+, -}(x)), x \in Y_0^{+, -}. \tag{24}$$

The results in the *Lemma* show that the characteristic flows $C_{-, -}^*(\cdot, \cdot)$ and $C_{+, -}^*(\cdot, \cdot)$ are invertible and define the smooth partial proper value function:

$$W_0(x) = \begin{cases} W_0^{-, -}(x) = V(\widehat{B}^{-, -}(x)) = -\widehat{\xi}_1^{-, -}(x), & x \in Y_0^{-, -} \\ W_0^{+, -}(x) = V(\widehat{B}^{+, -}(x)) = -\widehat{\xi}_1^{+, -}(x), & x \in Y_0^{+, -}. \end{cases} \tag{25}$$

Moreover, it follows that the corresponding admissible controls are given by:

$$\tilde{u}(x) = \begin{cases} \tilde{u}^{-, -}(x) = \arctan \left[\frac{\widehat{q}_2^{-, -}(x)\widehat{t}^{-, -}(x) - \widehat{q}_4^{-, -}(x)}{\widehat{t}^{-, -}(x) - \widehat{q}_3^{-, -}(x)} \right], & x \in Y_0^{-, -} \\ \tilde{u}^{+, -}(x) = \arctan \left[\frac{\widehat{q}_2^{+, -}(x)\widehat{t}^{+, -}(x) - \widehat{q}_4^{+, -}(x)}{\widehat{t}^{+, -}(x) - \widehat{q}_3^{+, -}(x)} \right], & x \in Y_0^{+, -}. \end{cases} \tag{26}$$

Theorem 1. *The corresponding admissible controls $\tilde{u}(\cdot)$ in (26) are optimal for the restriction on its domain $Y_0^{-, -} \cup Y_0^{+, -}$.*

Competing interests

The authors declare that they have no competing interests.

Authors' contributions

All authors have contributed to all parts of the article. All authors read and approved the final manuscript.

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